ERRATA

Chapter	Page	Location	Issue
1	9	Line 27	…especially Chapter 7, more will be said about SigmaAll and SigmaD. Should be Chapter 6.
3	89	Last line	…calculate the %EL for the three stainless steels. This makes no sense.
3	109	Eqns. 3.13 - 3.16	These equations are from the AISC Manual of Steel Construction Allowable Stress Design, and apply to six grades of structural steel, not all "ferrous and nonferrous metals". Shigley 7thEd gives these as Equations (1-3) and acknowledges AISC as the source, and states that this is "not a general approach". See separate discussion. Just use ns = Sy/SigmaDesign.
3	142	Recommended Reading	M. J. Ashby should be M. F. Ashby
4	164	Eqns. 4.37 & 4.40	Even though on page 147, h sub p is defined as Watts, in this equation it is Horsepower. Later, in Eqns. 4.41 & 4.42, it is back to being Watts. Why use h sub p for Watts?
4	179	Table of Resultant maximum stress for Axial Loading	P/A should be 50/0.7854 instead of 75/0.7854
6	227	Fig. 6.1	a & b don't agree with text just after Eqn. 6.2 describing them both as half-lengths.
6	238	Eqn. 6.5	K sub ci should be K sub Ic, where the Roman numeral I refers to Mode one cracking shown in Figure 6.9. Appendix C, page 962, correctly gives the stress intensity factors as K sub I. This should be consistent.
6	239	Table 6.1 Middle column heading	"Yield stress" should be "Yield Strength"
6	243	Line 4	Sy = yield stress of material. Should say "yield strength"
6	246	End of Example 6.6	SigmaE = 322.93 MPa, not 322.6 MPa.
7	284	Ex. 7.3 Solution	Figs 6.9(b) & (c) should be Figs 6.6(b) & (c)
7	285	Fig. 7.10a	The Ground and As Forged curves are NOT correct as plotted.
7	286	Eqn. 7.22	The metric version should be kf = 1.2484 d ^-0.112 to be the same as the English version.
9	376	Line 2	"defined" should be "divided"
9	382	Line 2	"slenderness ratio" should be "critical slenderness ratio". This is given correctly on page 383, line 7. Should also be corrected in the Symbols on page 374. The slenderness ratio is L over rg.
9	387	Design of Columns step 1.	Eqn. 9.15 doesn't need cross section or length, just E and Sy.
11	435	Symbols	Ssy, Su, Sut, and Sy should all be "strengths" not "stresses"
11	436	Line 22	"torsional movement" should be "torsional moment"
11	438	Fig. 11.2b	The M should be T.
11	438	Fig. 11.2c	The T should be M.
12	517	Fig 12.23	The vertical label needs a division "/" after the q.
12	518	Fig 12.24	The vertical label needs a division "/" after the Wr.
14	624	Section 14.6 Heading	Heading says "Interference", but it is not mentioned in the section.
14	628	Fig. 14.15	The teeth on Gear 2 are drawn wrong. They should look like the teeth on the ring in Fig. 14.19.
14	647	Line 20	Table 14.7 gives … assuming a pressure angle of 20°…. Values are for a Pressure Angle of 14.5°.
14	648	Table 14.7	Values are for a Pressure Angle of 14.5°.
15	694	Second to last line	"amgular" should be "angular"
16	726	Eqns. 16.21, 16.22, & 16.23	Variable Lt is used in all these equations, but means different things. In 16.21 it is the length of the threads under tension. In 16.22 and 16.23 it is the total threaded length on the bolt. Very different, yet the same variable. Maybe use Ltot for total threaded length.
16	740	Eqn. 16.48	This is a vectorial sum, so must show vector notation over each of the stresses.
16	744	Fig. 16.20	Depth of preparation should be Depth of penetration.
16	746	Eqn. 16.54	This is a vectorial sum, so must show vector notation over each of the stresses.
16	747-748	Table 16.12	The middle column has a variable given as Iu, unit moment of inertia, but it is really Zu, unit section modulus. To be convinced, consider that the moment of inertia does not differ from top to bottom of a vertically non-symmetric section, but section modulus does because the distance to the far fiber is different at the top and bottom.
16	747	Eqn. 16.55	Should be Z = te Zu = 0.707 he Zu
16	749	Line 1	Change "unit area moment of inertia" to "unit section modulus"
16	749	Eqn. 16.57	Should now read Sigma = M / Z
16	747	Table 16.12, last row	Denominator in X bar should be 2b + d, not 2 (b+d)
16	748	Table 16.12, last row	A = pi b should be A = pi d.
17	780	kθ	Units are N·m/Rev, not N/m
17	783	Table 17.1, second data row	Modulus of ASTM A227 should be 30 million, not 20 million.
17	783	Table 17.2	It's Chromium silicon, not Chromium silicone.
18	831	Just before Eqn. 18.6	Wear rate should be proportional to RATE OF work or energy.
18	833	Line 1	"…implies that a larger area …" should read "smaller" area. Large radius ratio puts ri close to ro, resulting in a narrow ring with a small area.
19	877	Line 1	"horsepower" should be Watts.
19	884	Table 19.4	Table is glitchy - Correction factor for 35° and 40° are both 0.89
19	899	Table 19.11	Note that units of transmitted power are Horsepower.
App. C	962	Eqns. C.2 and C.3	Neither a or W are defined.
App. C	962	Eqn. C.4	This doesn't match any curve on Figure C.3. For example, putting in lc/b = 0.4 gives Y = 3.73, not near any plotted value at lc/b = 0.4. It is off by a factor of about the square root of pi.
App. C	963	Figs. C.1, C.2, C.3 & C.5	Why is Sigma shown as edge forces?
App. C	965	Eqn. C.7	This doesn't match any curve on Figure C.4. For example, putting in lc/b = 0.4 gives Y = 1.98, not near any plotted value at lc/b = 0.4. The curves are completely different shapes.